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BRIEF INSTRUCTIONS FOR SIMBAT A COMPUTER PACKAGE FOR
UNCONDITIONAL AND CO. (U) BORGHAN (LEON E) INC LARAMIE
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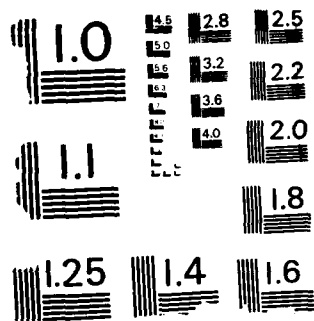
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March 1989

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Contract Report

An Investigation Conducted by
Leon E. Borgman, Inc., Laramie, WY

Sponsored by Mineral Management Service
Reston, VA

Brief Instructions for Subroutine SIMBAT, A Computer Package for Unconditional and Conditional Simulation of Ocean Wave Kinematics

ABSTRACT SIMBAT is a FORTRAN subroutine for computer simulation of ocean wave kinematics. Given an estimate of directional wave spectrum, the program calculates kinematics in the irregular wave field. These calculations can be conditioned on a particular kinematic or surface elevation time series. Brief instructions for use of SIMBAT are given.

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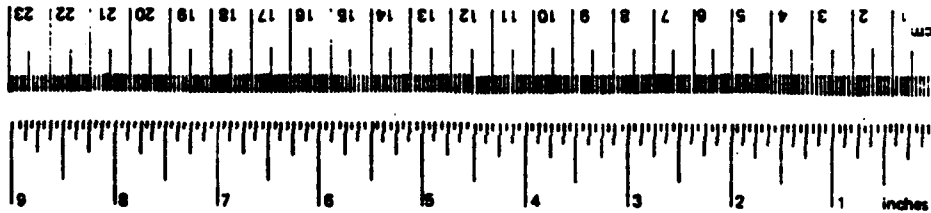
METRIC CONVERSION FACTORS

Approximate Conversions to Metric Measures

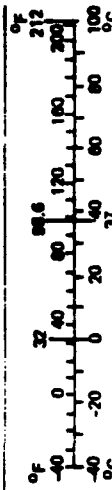
Symbol	When You Know	Multiply by	To Find	Symbol
in ft yd mi	inches	2.5	centimeters	cm
	feet	30	centimeters	cm
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	miles	1.6	kilometers	km
in ² ft ² yd ² mi ²	square inches	6.5	square centimeters	cm ²
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	square yards	0.8	square meters	m ²
	square miles	2.6	square kilometers	km ²
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	pounds	0.45	kilograms	kg
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	tablespoons	15	milliliters	ml
	fluid ounces	30	milliliters	ml
	cups	0.24	liters	l
	pints	0.47	liters	l
	quarts	0.95	liters	l
	gallons	3.8	liters	l
	cubic feet	0.03	cubic meters	m ³
	cubic yards	0.76	cubic meters	m ³
°F	Fahrenheit temperature	5/9 (after subtracting 32)	Celsius temperature	°C

Approximate Conversions from Metric Measures

When You Know	Multiply by	To Find	Symbol
LENGTH			
millimeters	0.04	inches	in
centimeters	0.4	inches	in
meters	3.3	feet	ft
meters	1.1	yards	yd
kilometers	0.6	miles	mi
AREA			
square centimeters	0.16	square inches	in ²
square meters	1.2	square yards	yd ²
square kilometers	0.4	square miles	mi ²
hectares (10,000 m ²)	2.5	acres	
MASS (weight)			
grams	0.035	ounces	oz
kilograms	2.2	pounds	lb
tonnes (1,000 kg)	1.1	short tons	
VOLUME			
milliliters	0.03	fluid ounces	fl oz
liters	2.1	pints	pt
liters	1.06	quarts	qt
liters	0.26	gallons	gal
cubic meters	36	cubic feet	ft ³
cubic meters	1.3	cubic yards	yd ³
TEMPERATURE (exact)			
°C	Celsius temperature	9/5 (then add 32)	Fahrenheit temperature °F



*1 in = 2.54 (exactly). For other exact conversions and more detailed tables, see NBS Mon. Publ. 286, Unit of Weights and Measures, Price \$2.25, SD Catalog No. C13 10 286.



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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER CR 89.007	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Brief Instructions for Subroutine SIMBAT, A Computer Package for Unconditional and Conditional Simulation of Ocean Wave Kinematics		5. TYPE OF REPORT & PERIOD COVERED Final Jul 1986 - May 1988
7. AUTHOR(s) Dr. Leon E. Borgman, Professor, University of Wyoming		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Leon E. Borgman, Inc. 2526 Park Ave Laramie, WY 82070		8. CONTRACT OR GRANT NUMBER(s) N62583/6203-3560
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Civil Engineering Laboratory Port Hueneme, CA 93043-5003		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS Conditional Wave Model JO 4804401
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) Mineral Management Service ATTN: Charles Smith Technology Assessment & Research Branch 12203 Sunrise Valley Dr; MS 647 Natl Cen		12. REPORT DATE March 1989
16. DISTRIBUTION STATEMENT (of this Report) Reston, VA 22091		13. NUMBER OF PAGES 50
15. SECURITY CLASS. (of this report) Unclassified		
18. DECLASSIFICATION DOWNGRADING SCHEDULE		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report) Approved for public release; distribution is unlimited.		
19. SUPPLEMENTARY NOTES Points of Contact: Naval Civil Engineering Laboratory Robert Zueck or David Shields, Ocean Structures Division		
20. KEY WORDS (Continue on reverse side if necessary and identify by block number) ocean waves, wave kinematics, conditional simulation; Legendre orthogonal polynomials; wave spectra		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) SIMBAT is a FORTRAN subroutine for computer simulation of ocean wave kinematics. Given an estimate of directional wave spectrum, the program calculates kinematics in the irregular wave field. These calculations can be conditioned on a particular kinematic or surface elevation time series. Brief instructions for use of SIMBAT are given. Sample runs are included in the appendix.		

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EXECUTIVE SUMMARY

As the title suggests this document provides brief instructions for a set of computer subroutines called SIMBAT. SIMBAT can unconditionally and conditionally simulate random directional ocean wave properties. Given an estimate of the directional wave spectrum, the program calculates elevations, kinematics, and pressures in the random wave field. These calculations can be conditioned on particular kinematic or surface elevation time series.

Conditional simulation of wave property time series statistically consistent with a specified measurement set, provides a very powerful approach to certain ocean engineering problems. The usual computer simulation of waves satisfying a specified model for the directional spectral density suffers from a serious practical defect if one is primarily interested in producing very large waves. Most simulations produce only average waves unless the simulation is run for a very, very long time. SIMBAT allows for the inclusion of a large wave profile or wave group to be embedded into the wave train, resulting in very short computer simulations.

The report describes basic wave properties in their complex form, describes the program SIMBAT, and explains in detail the development of the Legendre polynomials for storage of the large volume of wave kinematic data generated.

This contract report was prepared by Dr. Leon Borgman, professor of Statistics and Geology at the University of Wyoming, working for the Naval Civil Engineering Laboratory through his statistical consulting firm, Leon E. Borgman, Inc. The work was principally funded by the Mineral Management Service through Charles Smith of the Technology Assessment & Research Branch. Additional work in fiscal year 1990 is planned under Naval Facilities Engineering Command funding for testing, modifying, and annotating SIMBAT.



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1.0 GENERAL COORDINATE SYSTEM

The ocean wave kinematics will be referenced to a general horizontal coordinate system. All horizontal coordinate axes are established within navigation headings measured clockwise from true north.

θ_x = direction of positive x-axis

θ_y = direction of positive y-axis (1)

$$|\theta_x - \theta_y| = 90^\circ$$

Let the vertical axis z be zero at mean water level and positive downward.

The direction of travel of a wave is θ in navigation heading. The wave is traveling toward direction θ if $\beta_o = 1$ and is coming from direction θ if $\beta_o = -1$.

2.0 BASIC WAVE PROPERTIES

Eight wave properties are of interest. In terms of real functions, there are

(1) The water level elevation:

$$\eta(x,y,t) = a \cos \{ \beta_o k [x \cos(\theta - \theta_x) + y \cos(\theta - \theta_y)] - 2\pi ft - \phi \} \quad (2)$$

(2) The components of water particle velocity:

$$\begin{bmatrix} v_x(x,y,z,t) \\ v_y(x,y,z,t) \end{bmatrix} = a(2\pi f) \frac{\cosh[k(d-z)]}{\sinh(kd)} \begin{bmatrix} \beta_o \cos(\theta - \theta_x) \\ \beta_o \cos(\theta - \theta_y) \end{bmatrix} \cdot \cos \{ \beta_o k [x \cos(\theta - \theta_x) + y \cos(\theta - \theta_y)] - 2\pi ft - \phi \} \quad (3)$$

$$V_z(x,y,z,t) = a(2\pi f) \frac{\sinh[k(d-z)]}{\sinh(kd)} \sin[\beta_o k \{x \cos(\theta-\theta_x) + y \cos(\theta-\theta_y)\} - 2\pi ft - \phi] \quad (4)$$

(3) The components of water particle acceleration:

$$\begin{aligned} \begin{bmatrix} a_x(x,y,z,t) \\ a_y(x,y,z,t) \end{bmatrix} &= a(2\pi f)^2 \frac{\cosh[k(d-z)]}{\sinh(kd)} \begin{bmatrix} \beta_o \cos(\theta-\theta_x) \\ \beta_o \cos(\theta-\theta_y) \end{bmatrix} \\ &\cdot \sin[\beta_o k \{x \cos(\theta-\theta_x) + y \cos(\theta-\theta_y)\} \\ &- 2\pi ft - \phi] \end{aligned} \quad (5)$$

$$\begin{aligned} a_z(x,y,z,t) &= -a(2\pi f)^2 \frac{\sinh[k(d-z)]}{\sinh(kd)} \cos[\beta_o k \{x \cos(\theta-\theta_x) \\ &+ y \cos(\theta-\theta_y)\} - 2\pi ft - \phi] \end{aligned} \quad (6)$$

(4) The water pressure anomaly (plus and minus about hydrostatic pressure):

$$\begin{aligned} p(x,y,z,t) &= \rho g \frac{\cosh[k(d-z)]}{\cosh(kd)} \cos[\beta_o k \{x \cos(\theta-\theta_x) \\ &+ y \cos(\theta-\theta_y)\} - 2\pi ft + \phi] \end{aligned} \quad (7)$$

In these formulas

a = wave amplitude

f = wave frequency

d = water depth

k = wave number = $2\pi/\text{wavelength}$

ϕ = wave phase

ρ = water density

g = acceleration due to gravity

3.0 WAVE PROPERTIES IN COMPLEX FORM

Through the use of the complex form of $\cos \alpha$ and $\sin \alpha$ where

$$\cos \alpha = \frac{\exp(i\alpha) + \exp(-i\alpha)}{2} \quad (8)$$

$$\sin \alpha = \frac{\exp(i\alpha) - \exp(-i\alpha)}{2i} \quad (9)$$

All of the wave properties listed above can be expressed in the form:

$$B(f) = \frac{ae^{i\phi}}{2} G(z) T(f) H(\theta) \exp[-i\beta_o k \{x \cos(\theta - \theta_x) + y \cos(\theta - \theta_y)\}] \exp(i2\pi ft) \quad (10)$$

for positive f . The original real-valued wave time property equals $B(f) + B(f)^*$ where

$$B^*(f) = \text{complex conjugate of } B(f) \quad (11)$$

The functions G , T , and H for each wave property are:

(1) Water level elevation:

$$G(z) = T(f) = H(\theta) \equiv 1.0 \quad (12)$$

(2) Velocity:

$$G(z) = \begin{cases} \frac{\cosh[k(d-z)]}{\sinh(kd)} = \frac{\{e^{-kz} + e^{-k(2d-z)}\}}{\{1 - e^{-2kd}\}}, & \text{for } V_x \text{ and } V_y \\ \frac{\sinh[k(d-z)]}{\sinh(kd)} = \frac{\{e^{-kz} - e^{-k(2d-z)}\}}{\{1 - e^{-2kd}\}}, & \text{for } V_z \end{cases} \quad (13)$$

$$T(f) = \begin{cases} 2\pi f, & \text{for } V_x \text{ and } V_y \\ 2\pi fi, & \text{for } V_z \end{cases} \quad (14)$$

$$H(\theta) = \begin{cases} \beta \cos(\theta - \theta_x), & \text{for } V_x \\ \beta \cos(\theta - \theta_y), & \text{for } V_y \\ 1.0, & \text{for } V_z \end{cases} \quad (15)$$

(3) Acceleration:

$$G(z) = \begin{cases} \frac{\cosh[k(d-z)]}{\sinh(kd)} = \frac{\{e^{-kz} + e^{-k(2d-z)}\}}{\{1 - e^{-2kd}\}}, & \text{for } a_x \text{ and } a_y \\ \frac{\sinh[k(d-z)]}{\sinh(kd)} = \frac{\{e^{-kz} - e^{-k(2d-z)}\}}{\{1 - e^{-2kd}\}}, & \text{for } a_z \end{cases} \quad (16)$$

$$T(f) = \begin{cases} (2\pi f)^2 i, & \text{for } a_x \text{ and } a_y \\ -(2\pi f)^2, & \text{for } a_z \end{cases} \quad (17)$$

$$H(\theta) = \begin{cases} \beta \cos(\theta - \theta_x), & \text{for } a_x \\ \beta \cos(\theta - \theta_y), & \text{for } a_y \\ 1.0, & \text{for } a_z \end{cases} \quad (18)$$

(4) Pressure anomaly:

$$G(z) = \frac{\cosh[k(d-z)]}{\cosh(kd)} = \frac{\{e^{-kz} + e^{-k(2d-z)}\}}{\{1 + e^{-2kd}\}} \quad (19)$$

$$T(f) = \rho g \quad (20)$$

$$H(\theta) = 1.0 \quad (21)$$

4.0 WAVE PROPERTIES AS A DISCRETE FOURIER TRANSFORM

Let $ae^{i\theta}$ be replaced by the complex-valued wave amplitude A_{mj} for frequencies, f_m :

$$\left\{ m \Delta f; \quad 1 \leq m \leq \frac{N}{2} - 1 \right\} \quad \text{and} \quad \text{directions, } \theta_j,$$

$$\{ j \Delta \theta; \quad 1 \leq j \leq J \}$$

where $\Delta \theta = 2\pi/J$

$$\Delta f = 1/(N \Delta t)$$

Δt = time increment

$N \Delta t$ = length of time series

Also let k be replaced by k_m where

$$(2\pi f_m^2) = g k_m \tanh(k_m d) \quad (22)$$

The sequence, defined above for $1 \leq m < N/2$, can be extended to $N/2 < m \leq N-1$ by requiring that (in analogy to Eq 10)

$$B[(N-m)\Delta f] = B(m \Delta f)^* \quad (23)$$

where $B(f)$ is the general complex-valued wave property defined previously. The sum of these wave forms over $0 \leq m \leq N-1$ gives a discrete Fourier transform version of the wave properties. Here, it is assumed that $A_{mj} = 0$ for $m = 0$ and $m = N/2$. The $m = 0$ value is the mean or DC component. Taking it as zero guarantees that the wave property oscillates about zero. The value at $m = N/2$ is a very high frequency component at the Nyquist frequency. The length of the time series, N , and the time increment, Δt , can always be selected so that there is no energy at $f_{N/2} = (N/2) \Delta f$.

Then,

$$\left\{ \begin{array}{l} \text{wave property} \\ \text{at } t = n \Delta t \end{array} \right\} = \sum_{m=0}^{N-1} \left[\sum_{j=1}^J A_{mj} G_m T_m H_j \right. \\ \left. \cdot e^{-i\beta_0 k_m \{x \cos(\theta_j - \theta_x) + y \cos(\theta_j - \theta_y)\}} \right] e^{i2\pi \frac{mn}{N}} \quad (24)$$

This represents a summing of many waves, each with their own frequency, phase, and direction.

The last equation provides the general procedure for frequency-domain wave simulation. The quantity in the bracket is computed for $1 \leq m < N/2$. Usually this is only necessary for a relatively small subset of the interval, say

$$0 < m_B \leq m \leq m_L < N/2 \quad (25)$$

or

$$\text{NUM} = m_L - m_B + 1 \quad (26)$$

frequency increments. Then the rest of the coefficients for $0 \leq m \leq N/2$ are set to zero. The values for $N/2 < m \leq N-1$ are the complex conjugate of those in the left half of the sequence. That is,

$$\{\text{coefficient at } N-m\} = \{\text{coefficient at } m\}^* \quad (27)$$

5.4 PROGRAM LAYOUT

The program has seven options in addition to exit and help options. These are:

(1) Option No. 1.

A complex-valued matrix of wave amplitudes in the form:

$$A(m,j) = \rho(m,j) e^{i\phi(m,j)}$$

is simulated by frequency-domain computations. Here, ρ is the wave amplitude, ϕ is the phase. The m -index ranges over a regular grid of frequencies, and the j -index ranges over direction of wave travel. This option gives an unconditional simulation.

(2) Option No. 2.

A conditional simulation is a time series simulation which is forced to agree with a specified initial data time series segment, while maintaining appropriate correlated randomness. The program SIMBAT develops conditional simulation by several methods, all based on first producing a conditional simulation of the $A(m,j)$ described under the first option. These $A(m,j)$ however are conditionally simulated, rather than unconditionally simulated. The production of such a set of conditional simulation requires a number of pre-computed arrays. Option

No. 2 develops these input arrays. Thus, it is a pre-processor to the various options which subsequently compute the actual conditional simulations.

(3) Option No. 3.

This option uses the output from the previous option, for the case where the conditioning interval is shorter than the full time series, to compute a conditional simulation of the $A(m,j)$ complex matrix of wave amplitudes.

(4) Option No. 4.

This option is the same as Option No. 3 above, except that the conditioning interval is a full time series. That is, a measured time series of length, N , is used to develop the $A(m,j)$ complex-valued wave amplitude, which in turn may be used to simulate in a later option, time series of length, N .

(5) Option No. 5.

This option uses the complex amplitude table of $A(m,j)$ values to generate full time series (of length N) for various wave properties as specified. It basically is designed to be useful for the case where only a few time series (say 20 or less) are needed.

(6) Option No. 6.

This option is the fastest way to develop velocities and accelerations at many load points throughout a complex structure. It provides orthogonal polynomial coefficients for a Legendre expansion of each of eight wave properties (n , V_x , V_y , V_z , a_x , a_y , a_z , pressure) within a region $(x_0 - D_1 < x < x_0 + D_1)$, $(y_0 - D_2 < y < y_0 + D_2)$, and $0 < z < d$. A different, (optional) set of coefficients are provided at time step, as stored on a file. Option No. 6 computes these coefficients and stores

them on a master file. The user then reads the master file, time-step by time-step, and uses coefficients at that time step to generate all the wave kinematics at the various (x,y,z) locations throughout the structure. Then the user reads the next coefficient set at that time step, and so forth.

(7) Option No. 7.

This option provides a short list of wave amplitudes, phases, frequencies, wave numbers, and travel directions which give a wave train that approximates the full wave field represented by the $A(m,j)$ matrix. It will not exactly agree with the condition set, but will be somewhat near. It is probably slower also, in use, than Option No. 6 above.

An overall flow chart is shown in Figure 1. The delta stretching is applied by the user as based on having the sea surface elevation and the wave kinematics at the same (x,y) location. Other spectral models and spreading functions will also be coded into the package. Currently, the Ochi-Hubble and Gaussian spreading function are implemented. However, it is easy to insert other choices as subroutines into the structure.

It is anticipated that many further enhancements and modifications will be introduced during July and August 1988 as a natural outgrowth of experience and further needs as the program is used in applications.

6.0 SIMBAT SEPARATE-MODULE PACKAGE

The SIMBAT simulation package is also provided in separate modules of relatively small size for computation on larger microcomputers. The modules are:

1. SIM125 -- options 1, 2, and 5
2. SIM3 -- option 3
3. SIM4 -- option 4
4. SIM6 -- option 6
5. SIM7 -- option 7

Before running program: Set parameters and compile, either for unconditional simulation (option no. 1) or conditional simulations (option no. 2)

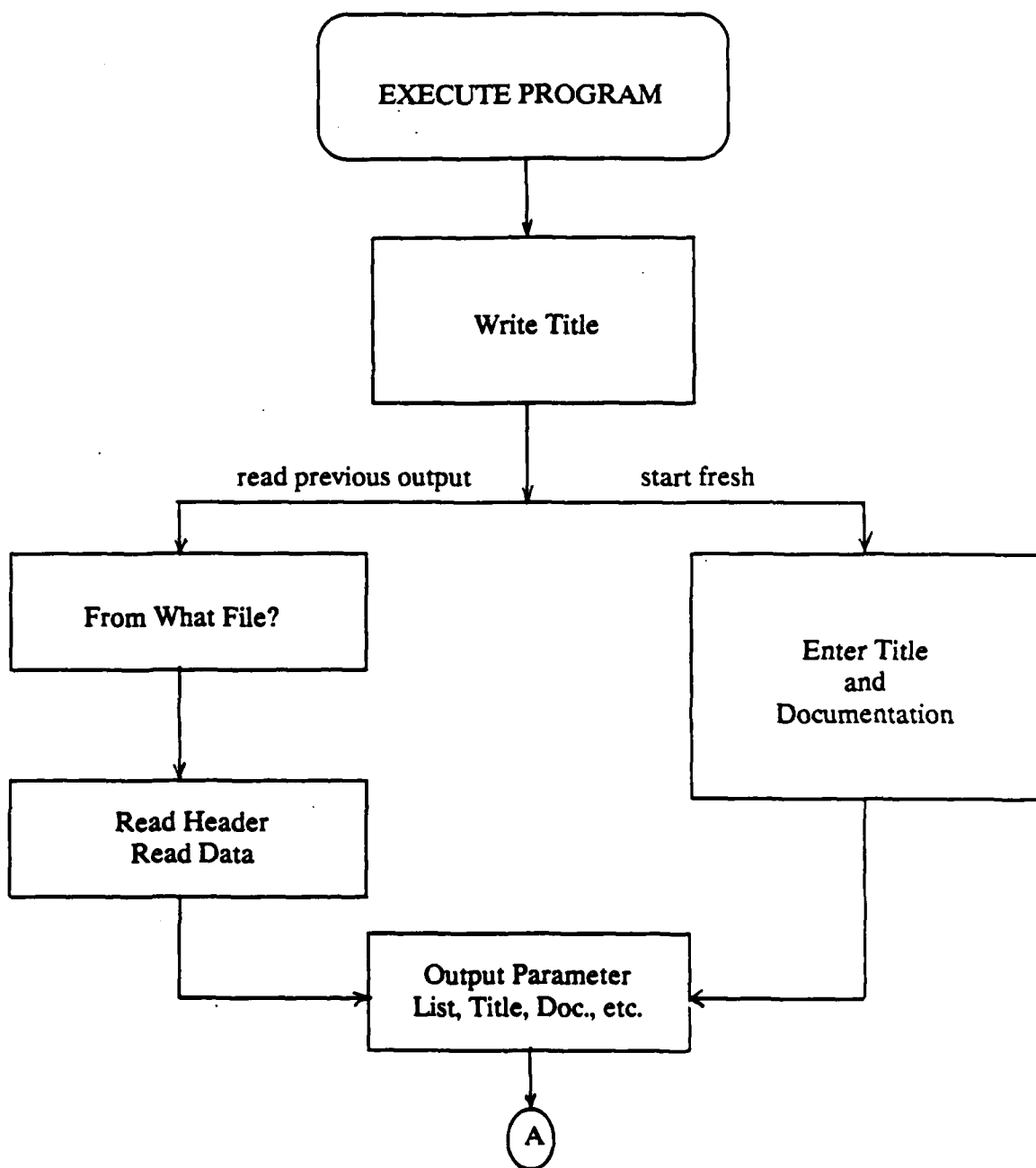


Figure 1. Overall flow chart for SIMBAT.FOR.

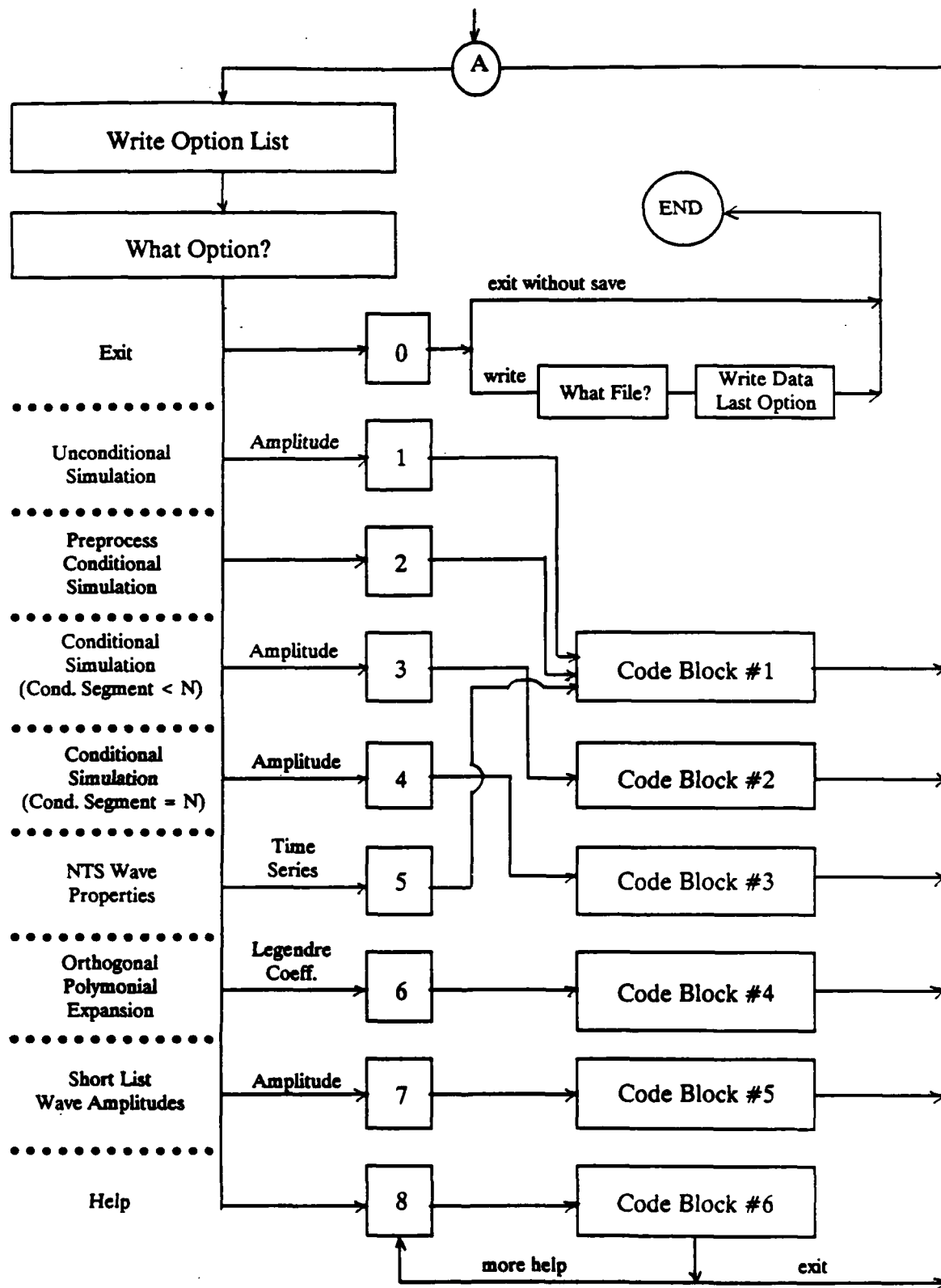
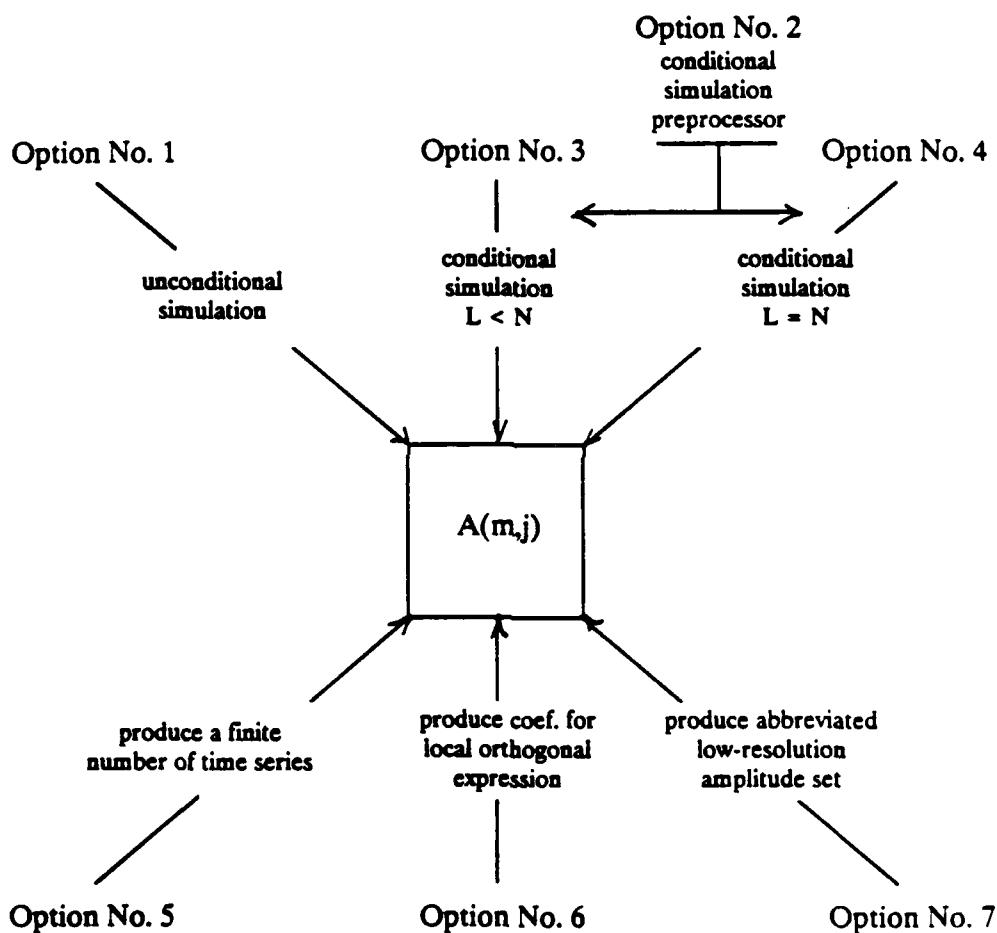


Figure 1. Overall flow chart for SIMBAT.FOR (continued).

Each module is used by executing the module and exiting with storage of the results on a user-selected file. The set of complex wave amplitudes

$$\{A(m,j) ; \quad 0 \leq m \leq N-1, \quad 0 \leq j \leq J-1\}$$

Each option can be classified relative to its relation to $A(m,j)$ as shown in Figure 2.



Option Nos. 1, 3, and 4 produce a set of $A(m,j)$. Option Nos. 5, 6, and 7 use an amplitude matrix as input and produce time series or algorithms to lead to time series. Option 2 is a special preprocessor which must precede the execution of Option Nos. 3 or 4.

Figure 2. SIMBAT module relationship.

Any of the basic inputs (1), (2,3), or (2,4) can be combined with any of the basic outputs (5), (6), or (7). Typical example runs are shown in Appendix A and as files on the accompanying diskettes. The fundamental output for Option No. 6 is given on the diskette as file MAST6.DAT. Option No. 6 requires further theoretical discussion. Similarly, the concepts of conditional probability deserve an expanded exposition.

7.0 ORTHOGONAL EXPANSION (OPTION 6)

The sheer mass of computations required to compute forces at many load points in a moving structure subject to wave actions is a major problem in operating with either conditional or unconditional simulations of wave kinematics. One approach is to try to reduce the number of waves required to produce (approximately) the same wave train. This is provided by Option No. 7. Another approach is to summarize the local variations of the wave kinematics in some sort of additive function system. Option No. 6 is based on Legendre and shifted Legendre orthogonal polynomials. Let

$$p_n(x) = a_0 + a_1x + \dots + a_nx^n \quad (28)$$

$$p_n^*(x) = a_0^* + a_1^*x + \dots + a_n^*x^n \quad (29)$$

be the Legendre and shifted Legendre orthogonal polynomials of order n . The coefficients are selected so that

$$\int_{-1}^1 p_m(x) p_n(x) dx = \begin{cases} 0 & , \text{ if } m \neq n \\ \frac{2}{2n+1} & , \text{ if } m = n \end{cases} \quad (30)$$

$$\int_0^1 p_m^*(x) p_n^*(x) dx = \begin{cases} 0 & , \text{ if } m \neq n \\ \frac{1}{2n+1} & , \text{ if } m = n \end{cases} \quad (31)$$

The first several Legendre polynomials are

$$p_0(x) = 1$$

$$p_1(x) = x$$

$$p_2(x) = (3x^2 - 1)/2$$

$$p_3(x) = (5x^3 - 3x)/2$$

$$p_4(x) = (35x^4 - 30x^2 + 3)/8$$

$$p_5(x) = (63x^5 - 70x^3 + 15x)/8$$

The SIMBAT programs incorporate Legendre polynomials up to order 12. Most approximations to wave kinematics will not require orders greater than 5.

The use of orthogonal polynomials to approximate an arbitrary function, $g(x)$, defined on $(-1,1)$ can be illustrated as follows. Suppose the approximation to be used is

$$g(x) \approx \sum_{n=0}^N a_n p_n(x) \quad (33)$$

The coefficients a_n are chosen from a "least-squares" criterion. Let a_n be those values which minimize

$$Q = \int_{-1}^1 \left[g(x) - \sum_{n=0}^N a_n p_n(x) \right]^2 dx \quad (34)$$

Then

$$\frac{\partial Q}{\partial a_k} = - \int_{-1}^1 2 \left[g(x) - \sum_{n=0}^N a_n p_n(x) \right] p_k(x) dx \quad (35)$$

$$\frac{1}{2} \left(\frac{\partial Q}{\partial a_k} \right) = - \int_{-1}^1 g(x) p_k(x) dx + \sum_{n=0}^N a_n \int_{-1}^1 p_n(x) p_k(x) dx \quad (36)$$

Q is at an extreme if $\partial Q / \partial a_k = 0$ for all $k=0,1,2,\dots,N$. This reduces to

$$\sum_{n=0}^N a_n \int_{-1}^1 p_n(x) p_k(x) dx = \int_{-1}^1 g(x) p_k(x) dx \quad (37)$$

But by the orthogonality relation, this further reduces to

$$a_k \left(\frac{2}{2k+1} \right) = \int_{-1}^1 g(x) p_k(x) dx \quad (38)$$

$$a_k = \left(\frac{2k+1}{2} \right) \int_{-1}^1 g(x) p_k(x) dx \quad (39)$$

The similar development for shifted Legendre polynomials gives

$$a_k^* = (2k+1) \int_0^1 g(x) p_k^*(x) dx \quad (40)$$

How can these relations be applied to ocean wave kinematics? The essential canonical form for a linear wave property is given in Equation 24. It should be noted that in every case, $G_m(z)$ is either 1.0 (water level elevation) or is of the form

$$\frac{e^{-k_m z} + s_1 e^{-k_m (2d-z)}}{1 + s_2 e^{-2k_m d}} \quad (41)$$

where k_m is the wave number. Thus, the general wave property, $p(n \Delta t)$ can be expressed from Equation 10 as

$$p(n \Delta t) = \sum_{m=0}^{N-1} C_m e^{i2\pi mn/N} \quad (42)$$

where C_m is the FFT coefficient given by

$$C_m = \sum_{j=1}^J A_{mj} e^{-i\beta_o k_m \{x \cos(\theta - \theta_x) + y \cos(\theta - \theta_y)\}} \quad (43)$$

for sea surface elevations, and

$$C_m = \sum_{j=1}^J A_{mj} T_m H_j \frac{\left\{ e^{-k_m z} + s_1 e^{-k_m(2d-z)} \right\}}{\left\{ 1 + s_2 e^{-k_m d} \right\}} e^{-i\beta_o k_m \{x \cos(\theta-\theta_x) + y \cos(\theta-\theta_y)\}} \quad (44)$$

for the other wave properties. These can be expressed as a sum of products of separate functions of x, y, and z as

Sea Surface

$$C_m = \sum_{j=1}^J A_{mj} e^{i\beta_o k_m x \cos(\theta-\theta_x)} e^{i\beta_o k_m y \cos(\theta-\theta_y)} \quad (45)$$

Other Wave Properties

$$C_m = \sum_{j=1}^J \frac{A_{mj} T_m H_j}{1 + s_2 e^{-k_m d}} \left\{ e^{-k_m z} + s_1 e^{-k_m(2d-z)} \right\} e^{-i\beta_o k_m x \cos(\theta-\theta_x)} e^{-i\beta_o k_m y \cos(\theta-\theta_y)} \quad (46)$$

Suppose it is desired to obtain a good representation locally in the vicinity of the structure. Consider the volume

$$\begin{aligned} x_o - D_1 &\leq x \leq x_o + D_1 \\ y_o - D_2 &\leq y \leq y_o + D_2 \\ 0 &\leq z \leq d \end{aligned} \quad (47)$$

(Here z has been taken as positive downwards and zero at mean water level.)

It is natural to scale the function as

Sea Surface

$$C_m = \sum_{j=1}^J A_{mj} e^{-i\beta_o k_m x_o \cos(\theta-\theta_x)} e^{-i\beta_o k_m D_1 \left(\frac{x-x_o}{D_1}\right) \cos(\theta-\theta_x)} e^{-i\beta_o k_m y_o \cos(\theta-\theta_y)} e^{-i\beta_o k_m D_2 \left(\frac{y-y_o}{D_2}\right) \cos(\theta-\theta_y)} \quad (48)$$

Other Wave Properties

$$C_m = \sum_{j=1}^J \frac{A_{mj} T_m H_j}{1 + s_2 e^{-2k_m d}} \left\{ e^{-k_m z} + s_1 e^{-k_m (2d-z)} \right\} e^{-i\beta_o k_m x_o \cos(\theta-\theta_x)} e^{-i\beta_o k_m D_1 \left(\frac{x-x_o}{D_1}\right) \cos(\theta-\theta_x)} e^{-i\beta_o k_m y_o \cos(\theta-\theta_y)} e^{-i\beta_o k_m D_2 \left(\frac{y-y_o}{D_2}\right) \cos(\theta-\theta_y)} \quad (49)$$

Let

$$e^{-i\beta_o k_m D_1 \left(\frac{x-x_o}{D_1}\right) \cos(\theta-\theta_x)} = \sum_{\alpha=0}^N a_{\alpha} p_{\alpha} \left(\frac{x-x_o}{D_1}\right) \quad (50)$$

$$e^{-i\beta_o k_m D_2 \left(\frac{y-y_o}{D_2}\right) \cos(\theta-\theta_y)} = \sum_{\beta=0}^N a_{\beta} p_{\beta} \left(\frac{y-y_o}{D_2}\right) \quad (51)$$

$$e^{-k_m z} = \sum_{\gamma=0}^N C_{\gamma} p_{\gamma}^*(e^{-k_o z}) \quad (52)$$

where k_o is a selected single reference wave number. For many applications, the second term

$$e^{-k_m(2d-z)}$$

is negligible because depth is large. For the moment suppose that this second term can be ignored. It will be reintroduced later. Then if

$$\begin{aligned} u &= (x-x_o)/D_1 \\ v &= (y-y_o)/D_2 \\ w_1 &= e^{-k_o z} \end{aligned} \quad (53)$$

Sea Surface

$$\begin{aligned} C_m &= \sum_{j=1}^J A_{mj} e^{-i\beta_o k_m [x_o \cos(\theta-\theta_x) + y_o \cos(\theta-\theta_y)]} \\ &\cdot \sum_{\alpha=0}^N a_{\alpha} p_{\alpha}(u) \cdot \sum_{\beta=0}^N b_{\beta} p_{\beta}(v) \end{aligned} \quad (54)$$

Other Wave Properties

$$\begin{aligned} C_m &= \sum_{j=1}^J \frac{A_{mj} T_m H_j e^{-i\beta_o k_m [x_o \cos(\theta-\theta_x) + y_o \cos(\theta-\theta_y)]}}{1 + s_2 e^{-2k_m d}} \\ &\cdot \sum_{\alpha=0}^N a_{\alpha} p_{\alpha}(u) \cdot \sum_{\beta=0}^N b_{\beta} p_{\beta}(v) \cdot \sum_{\gamma=0}^N c_{\gamma} p_{\gamma}^*(e^{-k_o z}) \end{aligned} \quad (54)$$

If this is substituted into Equation 42

$$p(n \Delta t) = \sum_{\alpha=0}^N \sum_{\beta=0}^N \sum_{\gamma=0}^N B_{\alpha, \beta, \gamma}(n \Delta t) p_{\alpha}(u) p_{\beta}(v) p_{\gamma}^*(e^{-k_o z}) \quad (55)$$

where (sea surface case)

$$B_{\alpha, \beta, \gamma}(n \Delta t) = \sum_{m=0}^{N-1} \left[\sum_{j=1}^J a_{\alpha} b_{\beta} A_{mj} e^{-i\beta_o k_m x_o \cos(\theta-\theta_x)} e^{-i\beta_o k_m y_o \cos(\theta-\theta_y)} \right] e^{i2\pi mn/N} \quad (56)$$

This is an FFT of the quantity within { } for each α , β , and γ combination.

The other wave properties have a similar expression with

$$B_{\alpha, \beta, \gamma}(n \Delta t) = \sum_{m=0}^{N-1} \left[\sum_{j=1}^J a_{\alpha} b_{\beta} c_{\gamma} A_{mj} T_m H_j \frac{e^{-i\beta_o k_m [x_o \cos(\theta-\theta_x) + y_o \cos(\theta-\theta_y)]}}{1 + s_2 e^{-2k_m d}} \right] e^{i2\pi mn/N} \quad (57)$$

At a given time, $n \Delta t$, many of the $B_{\alpha, \beta, \gamma}$, for a given wave property, are negligible. After all the region $x_o \pm D_1$ and $y_o \pm D_2$ is relatively small relative to the wave lengths. Hence low order polynomials are all that are required in order to represent the variation over the horizontal region. The variation vertically is more or less exponentially attenuated with depth, so a polynomial in

$$e^{-k_o z}$$

should only need relatively low order.

Hence, at a given time, only a few $B_{\alpha, \beta, \gamma}$ will be needed to represent the wave property. The particular coefficient needed may, however, be different from one time step to another.

Up to here the actual computation of a_α , b_β , and c_γ has been not explicitly stated. From the definition of orthogonal polynomials

$$a_\alpha = \frac{2\alpha+1}{2} \int_{-1}^1 e^{-ik_m \beta_o D_1 \cos(\theta-\theta_x)u} p_\alpha(u) du \quad (58)$$

$$b_\beta = \frac{2\beta+1}{2} \int_{-1}^1 e^{-ik_m \beta_o D_2 \cos(\theta-\theta_y)v} p_\beta(v) dv \quad (59)$$

$$c_\gamma = (2\gamma+1) \int_0^1 w_1^{k_m/k_o} p_\gamma^*(w_1) dw \quad (60)$$

8.0 IMPLEMENTATION IN CODE

The a_α , b_β , and c_γ , which are functions of m and j , are computed and combined as given in Equation 56 and 57 and then Fourier transform with the fast Fourier transform to develop $B_{\alpha,\beta,\gamma}(n \Delta t)$ for each wave property. These are sorted in order of absolute value at each time step and listed in a sequential file.

The coefficients are listed in the file in integer form with the last 3 digits giving an index which may be used to determine the orders α , β , and γ for that coefficient. Thus, the coefficient with value xxx.xxx is listed as the integer xxxxxxyyy where yyy is the order designator. A matrix

$$\text{LSTXYZ}(\text{yyy},1) = \alpha$$

$$\text{LSTXYZ}(\text{yyy},2) = \beta$$

$$\text{LSTXYZ}(\text{yyy},3) = \gamma$$

gives the order associated with each yyy value. The integers are ranked in order of decreasing absolute value. Thus the user can compute with the much abbreviated list of coefficients needed at that time step to represent the wave property within the local region.

9.0 OTHER DEPTH TERM

Let

$$w_2 = e^{-k_o(2d-z)}$$

Then an exactly similar expansion with the same coefficients can be developed. The resulting representation of the wave property is

$$p(n \Delta t) = \sum_{\alpha=0}^N \sum_{\beta=0}^N \sum_{\gamma=0}^N B_{\alpha,\beta,\gamma}(n \Delta t) p_{\alpha}(u) p_{\beta}(v) \cdot \left\{ p_{\alpha}^*(e^{-k_o z}) + s_1 p_{\alpha}^*(e^{-k_o(2d-z)}) \right\}$$

Note: The Module SIM6 is still under testing and may be changed further as the study continues.

Appendix A
EXAMPLE RUNS

**OPTION NO. 1 CONSOLE LISTING
TO BE FOLLOWED BY OPTION NO. 5**

PROGRAM SIMULATES WAVE PROPERTIES BY FREQUENCY DOMAIN METHODS
FOR EITHER UNCONDITIONAL OR CONDITIONAL SIMULATIONS.
(WRITTEN BY LEON BORGMAN, LARAMIE, WYOMING)

PLEASE KEY RETURN TO CONTINUE

DO YOU WISH TO READ OUTPUT FROM PREVIOUS RUNS
OF OPTIONS #1 OR #2? (Y = YES, N = NO)
N

ENTER A 50-CHARACTER TITLE FOR THE TIME SERIES DATA.

5/30/88 5:07 AM CONSOLE LIST EXAMPLE

ENTER A 50-CHARACTER SUMMARY OF THE TIME SERIES
DOCUMENTATION FOR FUTURE REFERENCE.

THE OUTPUT IS STORED ON L:LIST1.DAT
OPTIONS ACTIVE IN THIS SUBPROGRAM:

- 0. EXIT PROGRAM
- 1. PRODUCE COMPLEX AMPLITUDES FOR UNCONDITIONAL SIMULATIONS
- 2. PRE-PROCESS DATA TO PRODUCE NECESSARY INPUT FOR A
CONDITIONAL SIMULATION
- 5. SIMULATE TIME SERIES FROM AMPLITUDES (USES OUTPUT FROM
STEP #1, #3, OR #4.)
- 8. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

1 OPTION NO.

ENTER SPECTRAL-LINE CUTOFF FRACTION. (NOTE: A SMALL
VALUE IS GOOD. ONLY THOSE LINES GIVING VARIANCE CONTRIBUTION
GREATER THAN OR EQUAL TO (CUTOFF*LARGEST SPECTRAL LINE) ARE
KEPT

0.00001

ENTER SEED INTEGER FOR RANDOM NUMBER GENERATOR. I10

123456

ENTER IOPT:

IOPT=1 INDICATES DSPEC MATRIX IS COMPUTED AND THEN
STORED FOR FUTURE USE IN A USER-SPECIFIED FILE.
IOPT=2 INDICATES DSPEC MATRIX IS READ FROM A

WHAT IS YOUR CHOICE?

1

ENTER FILE NAME TO WHICH THE DATA IS TO BE STORED.

J:DSPEC1.DAT

ENTER A 50-CHARACTER TITLE FOR DRSPEC. MATRIX

EXAMPLE DIR. SPECTRA NO. 1

MODE NUMBER AT THIS STEP = 1

DO YOU WANT TO ENTER ANOTHER MODE?

ENTER N=NO IF NO MORE MODES ARE TO BE ENTERED.

OTHERWISE, ENTER Y=YES

WHAT IS YOUR CHOICE?

Y

ENTER LAMDA FOR O-H SPECTRA. NOTE: LAMDA=1.0 FOR

P-M SPECTRA OR JONSWAP SPECTRA

1.0

ENTER MODAL FREQUENCY FOR MODE.

0.1

ENTER TOTAL VARIANCE OF MODE.

VARIANCE DIMENSIONS DETERMINE SPECTRA DIMENSIONS

DR.SPECT.DENSITY WILL BE IN UNITS OF

LENGTH**2 PER (HERTZ-RADIAN)

100.0

PRINC.DIR.=PRINC.DIR.CONST.+

PRINC.DIR.SLOPE*(FREQ.-MODAL FREQ.)

DIMENSIONS: PRINC.DIR.CONST. IN NAV. DEGREES

PRINC.DIR.SLOPE IN DEGREES-SEC.

ENTER PRINCIPAL DIRECTION CONSTANT FOR MODE.

0.0

ENTER PRINCIPAL DIRECTION SLOPE FOR MODE.

0.0

SPRD.STD.DEV.=SPRD.STD.DEV.CONST.+

SPRD.STD.DEV.SLOPE*(FREQ.-MODAL FREQ.)

DIMENSIONS: SPRD.STD.DEV.CONST. IN NAV. DEGREES

SPRD.STD.DEV.SLOPE IN DEGREES-SEC.

ENTER SPREADING STD. DEV. CONSTANT FOR MODE.

30.0

ENTER SPREADING STD. DEV. SLOPE FOR MODE.

0.0

SPECTRA PARAMETERS: LAMDA, F0, VAR= 1.00000

.10000

100.0

SPREAD PARAMETERS: THET0, THET1, SIG0, SIG1= .00000

.00000

ARE THESE THE VALUES YOU WANTED? IF NOT, ENTER N=NO

AND RE-ENTER PARAMETERS FOR THIS MODE.

OTHERWISE ENTER Y=YES

WHAT IS YOUR CHOICE?

Y

MODE NUMBER AT THIS STEP = 2

DO YOU WANT TO ENTER ANOTHER MODE?

ENTER N=NO IF NO MORE MODES ARE TO BE ENTERED.

OTHERWISE, ENTER Y=YES

WHAT IS YOUR CHOICE?

N

AMPLITUDE RANDOMNESS MENU

1. RANDOM PHASE, BUT WAVE AMPLITUDE DETERMINISTIC AND
CONSTRAINED TO BE EQUAL TO $2.0 * \text{SQRT}(S(F, \text{THETA}))$

2. RANDOM PHASE AND RANDOM AMPLITUDE

PLEASE ENTER YOUR CHOICE

.....

POINT A REACHED
 POINT B REACHED
 POINT C REACHED
 POINT D REACHED
 NUMBER OF DEGREES OF FREEDOM = 1707
 OPTIONS ACTIVE IN THIS SUBPROGRAM:
 0. EXIT PROGRAM
 1. PRODUCE COMPLEX AMPLITUDES FOR UNCONDITIONAL SIMULATIONS
 2. PRE-PROCESS DATA TO PRODUCE NECESSARY INPUT FOR A
 CONDITIONAL SIMULATION
 3. SIMULATE TIME SERIES FROM AMPLITUDES (USES OUTPUT FROM
 STEP #1, #3, OR #4.)
 8. HELP

 (PLEASE ENTER YOUR CHOICE AND KEY RETURN)

 0
 DO YOU WANT TO SAVE THE OUTPUT FROM LAST OPTION
 STEP ON A SEPARATE USER SPECIFIED FILE ? Y OR N
 Y
 PLEASE ENTER THE FILE NAME FOR STORAGE
 J:OUT1.DAT **OUTPUT FILE**

 Programmed STOP

The printer listing is in file LIST1.DAT.
 The output to be used as input to Option no. 5 is stored in OUT2.DAT.

**CONSOLE LIST FOR OPTION NO. 5
FOLLOWING OPTION NO. 1**

PROGRAM SIMULATES WAVE PROPERTIES BY FREQUENCY DOMAIN METHODS
FOR EITHER UNCONDITIONAL OR CONDITIONAL SIMULATIONS.
(WRITTEN BY LEON BORGMAN, LARAMIE, WYOMING)

PLEASE KEY RETURN TO CONTINUE

DO YOU WISH TO READ OUTPUT FROM PREVIOUS RUNS
OF OPTIONS #1 OR #2? (Y = YES, N = NO

Y

WHAT IS THE FILE NAME FOR PREVIOUS OUTPUT?

J:OUT1.DAT

OPTIONS ACTIVE IN THIS SUBPROGRAM:

- 0. EXIT PROGRAM
- 1. PRODUCE COMPLEX AMPLITUDES FOR UNCONDITIONAL SIMULATIONS
- 2. PRE-PROCESS DATA TO PRODUCE NECESSARY INPUT FOR A
CONDITIONAL SIMULATION
- 5. SIMULATE TIME SERIES FROM AMPLITUDES (USES OUTPUT FROM
STEP #1, #3, OR #4.)
- 8. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

5 OPTION NO.

ENTER NOISE TO SIGNAL RATIO, AS RATIO OF NOISE
STANDARD DEVIATION TO SIGNAL STANDARD DEVIATION

0.0

CHANNEL NUMBER: 1

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.0

CHANNEL NUMBER: 2

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.0

CHANNEL NUMBER: 3

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.0

ENTER TIME STEP FOR START OF LIST AND RETURN

1

ENTER TIME STEP AT TERMINATION OF LIST AND RETURN

200

ENTER 0 IF GRAPHICAL OUTPUT IS DESIRED

KEY 1 IF NUMERICAL LIST OF TIME SERIES IS WANTED

0

NUMBER OF DEGREES OF FREEDOM = 0

OPTIONS ACTIVE IN THIS SUBPROGRAM:

1. PRODUCE COMPLEX AMPLITUDES FOR UNCONDITIONAL SIMULATIONS
2. PRE-PROCESS DATA TO PRODUCE NECESSARY INPUT FOR A
CONDITIONAL SIMULATION
5. SIMULATE TIME SERIES FROM AMPLITUDES (USES OUTPUT FROM
STEP #1, #3, OR #4.)
8. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

5
ENTER NOISE TO SIGNAL RATIO. AS RATIO OF NOISE
STANDARD DEVIATION TO SIGNAL STANDARD DEVIATION

0.0

CHANNEL NUMBER: 1

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.0

CHANNEL NUMBER: 2

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.0

CHANNEL NUMBER: 3

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.0

ENTER TIME STEP FOR START OF LIST AND RETURN

1

ENTER TIME STEP AT TERMINATION OF LIST AND RETURN

200

ENTER 0 IF GRAPHICAL OUTPUT IS DESIRED

KEY 1 IF NUMERICAL LIST OF TIME SERIES IS WANTED

1

NUMBER OF DEGREES OF FREEDOM = 0

OPTIONS ACTIVE IN THIS SUBPROGRAM:

0. EXIT PROGRAM

1. PRODUCE COMPLEX AMPLITUDES FOR UNCONDITIONAL SIMULATIONS

2. PRE-PROCESS DATA TO PRODUCE NECESSARY INPUT FOR A
CONDITIONAL SIMULATION

5. SIMULATE TIME SERIES FROM AMPLITUDES (USES OUTPUT FROM
STEP #1, #3, OR #4.)

8. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

DO YOU WANT TO SAVE THE OUTPUT FROM LAST OPTION
STEP ON A SEPARATE USER SPECIFIED FILE ? Y OR N
N **NO OUTPUT**

Programmed STOP

F>

CONSOLE LIST FOR PREPROCESSOR OPTION NO. 2

PROGRAM SIMULATES WAVE PROPERTIES BY FREQUENCY DOMAIN METHODS
FOR EITHER UNCONDITIONAL OR CONDITIONAL SIMULATIONS.
(WRITTEN BY LEON BORGMAN, LARAMIE, WYOMING)

PLEASE KEY RETURN TO CONTINUE

DO YOU WISH TO READ OUTPUT FROM PREVIOUS RUNS
OF OPTIONS #1 OR #2? (Y = YES, N = NO
N

ENTER A 50-CHARACTER TITLE FOR THE TIME SERIES DATA.

5/30/88 9:26 PM CONSOLE LIST FOR OPTION 2

ENTER A 50-CHARACTER SUMMARY OF THE TIME SERIES
DOCUMENTATION FOR FUTURE REFERENCE.

LIST OUTPUT STORED ON JL J:LIST2.DAT

OPTIONS ACTIVE IN THIS SUBPROGRAM:

0. EXIT PROGRAM
1. PRODUCE COMPLEX AMPLITUDES FOR UNCONDITIONAL SIMULATIONS
2. PRE-PROCESS DATA TO PRODUCE NECESSARY INPUT FOR A
CONDITIONAL SIMULATION
5. SIMULATE TIME SERIES FROM AMPLITUDES (USES OUTPUT FROM
STEP #1, #3, OR #4.)
9. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

2 OPTION NO.

ENTER SPECTRAL-LINE CUTOFF FRACTION. (NOTE: A SMALL
VALUE IS GOOD. ONLY THOSE LINES GIVING VARIANCE CONTRIBUTION
GREATER THAN OR EQUAL TO (CUTOFF*LARGEST SPECTRAL LINE) ARE
KEPT

0.000001

ENTER SEED INTEGER FOR RANDOM NUMBER GENERATOR. I10

1357934

ENTER IOPT:

IOPT=1 INDICATES DSPEC MATRIX IS COMPUTED AND THEN
STORED FOR FUTURE USE IN A USER-SPECIFIED FILE.

IOPT=2 INDICATES DSPEC MATRIX IS READ FROM A

```

*****
2
  POINT V REACHED
ENTER FILE NAME FROM WHERE THE DATA IS TO BE READ.
J:DSPEC1.DAT
  POINT W REACHED
  POINT X REACHED
  POINT Y REACHED
  POINT Z REACHED
*****
AMPLITUDE RANDOMNESS MENU
1.    RANDOM PHASE, BUT WAVE AMPLITUDE DETERMINISTIC AND
      CONSTRAINED TO BE EQUAL TO 2.0*SQRT(S(F,THETA))
2.    RANDOM PHASE AND RANDOM AMPLITUDE
PLEASE ENTER YOUR CHOICE
*****
2
  POINT B REACHED
  POINT C REACHED
  POINT D REACHED
NUMBER OF DEGREES OF FREEDOM = 1729
OPTIONS ACTIVE IN THIS SUBPROGRAM:
0. EXIT PROGRAM
1. PRODUCE COMPLEX AMPLITUDES FOR UNCONDITIONAL SIMULATIONS
2. PRE-PROCESS DATA TO PRODUCE NECESSARY INPUT FOR A
   CONDITIONAL SIMULATION
5. SIMULATE TIME SERIES FROM AMPLITUDES (USES OUTPUT FROM
   STEP #1, #3, OR #4.)
9. HELP
*****
(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

DO YOU WANT TO SAVE THE OUTPUT FROM LAST OPTION
STEP ON A SEPARATE USER SPECIFIED FILE ? Y OR N
J:OUT2.DAT

Programmed STOP

F>

```

Store output on OUT2.DAT.
Printer output is shown on LIST2.DAT.

1:51:43

CONSOLE LIST OPTION NO. 3

PROGRAM SIMULATES WAVE PROPERTIES BY FREQUENCY DOMAIN METHODS
FOR EITHER UNCONDITIONAL OR CONDITIONAL SIMULATIONS.
(WRITTEN BY LEON BORGMAN, LARAMIE, WYOMING)

PLEASE KEY RETURN TO CONTINUE

DO YOU WISH TO READ OUTPUT FROM PREVIOUS RUNS
BY OPTIONS #1 OR #2? (Y = YES, N = NO)
Y

WHAT IS THE FILE NAME FOR PREVIOUS OUTPUT?

J:OUT2.DAT INPUT

TITLE: 5/23/83

DOCUMENTATION: 6:20 PM

ISEED= 12345677 FCHUZ= 3 N= 512 NTS= :

OPTIONS ACTIVE IN THIS SUBPROGRAM:

0. EXIT PROGRAM

3. DEVELOP COMPLEX-VALUED AMPLITUDES, CONDITIONED ON GIVEN
INPUT, WHERE CONDITIONING INPUT IS LESS THAN N.
(USES OUTPUT FROM STEP #2.)

8. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

3 OPTION NO.

MENU FOR OPTION #3 CONDITIONING INPUT:

1. READ THE CONDITIONING TIME SERIES INTERVAL FROM A FILE.
2. INPUT FROM CONSOLE A SINGLE POINT CHECK COMPUTATION.

1

THE GIVEN TIME SERIES IS TO BE READ FROM WHAT FILE?

J:GTS3.DAT

AT A, XC(1,1,1)=+1.387074E+02

AT B, XC(1,1,1)=+1.387074E+02

ITER=1 ERROR=+2.87978591006331E-001

ITER=2 ERROR=+1.49614657795246E-001

ITER=3 ERROR=+8.33678097563081E-002

ITER=4 ERROR=+6.25658778317937E-002

ITER=5 ERROR=+4.79428186885693E-002

ITER=6 ERROR=+3.98655722717029E-002

ITER=7 ERROR=+4.07938739941164E-002

ITER=8 ERROR=+4.82520036410251E-002

ITER=9 ERROR=+4.01262099826422E-002

ITER=10 ERROR=+3.70754879940331E-002

ITER=11 ERROR=+3.61288061379002E-002

ITER=12 ERROR=+3.72097472419775E-002

ITER=14	ERROR=+4.35425370381022E-002
ITER=15	ERROR=+4.31572720665299E-002
ITER=16	ERROR=+3.65276807834511E-002
ITER=17	ERROR=+4.05862967637325E-002
ITER=18	ERROR=+4.50411327745454E-002
ITER=19	ERROR=+4.23025648241650E-002
ITER=20	ERROR=+3.22563850185996E-002
ITER=21	ERROR=+4.52897460582820E-002
ITER=22	ERROR=+5.80676454774573E-002
ITER=23	ERROR=+6.82274676210544E-002
ITER=24	ERROR=+8.50967519543853E-002
ITER=25	ERROR=+1.81105624147220E-001
ITER=26	ERROR=+1.77652397112268E-001
ITER=27	ERROR=+3.41351864835669E-002
ITER=28	ERROR=+4.44516861145773E-002
ITER=29	ERROR=+7.15560563985889E-002
ITER=30	ERROR=+4.29835306096395E-002
ITER=31	ERROR=+4.51449594922817E-002
ITER=32	ERROR=+4.19182391619607E-002
ITER=33	ERROR=+3.42203073397959E-002
ITER=34	ERROR=+4.77779413038873E-002
ITER=35	ERROR=+2.83636885652342E-002
ITER=36	ERROR=+4.15758046336139E-002
ITER=37	ERROR=+5.14872682905144E-002
ITER=38	ERROR=-5.46444103222024E-002
ITER=39	ERROR=+6.33359288827641E-002
ITER=40	ERROR=+6.23405431514012E-002
ITER=41	ERROR=+8.06736829722208E-002
ITER=42	ERROR=+4.95387506993048E-002
ITER=43	ERROR=-4.86191924249298E-002
ITER=44	ERROR=+1.49718831227054E-001
ITER=45	ERROR=-1.88103175338544E-001
ITER=46	ERROR=-1.94332103305322E-001
ITER=47	ERROR=+1.02469503219081E-001
ITER=48	ERROR=-8.90559065664480E-002
ITER=49	ERROR=+1.14525922226387E-001
ITER=50	ERROR=+2.24505272049408E-002
ITER=51	ERROR=-2.60558536876116E-002
ITER=52	ERROR=+7.11497511871963E-002
ITER=53	ERROR=+4.82351928834419E-002
ITER=54	ERROR=+2.25687866839736E-002
ITER=55	ERROR=+2.18595948253765E-002
ITER=56	ERROR=+8.37377339729528E-002
ITER=57	ERROR=+3.62731923206972E-002
ITER=58	ERROR=+2.85838936056325E-002
ITER=59	ERROR=+2.34223279212249E-002
ITER=60	ERROR=+1.54923490182749E-002
ITER=61	ERROR=-1.65379395479899E-002
ITER=62	ERROR=+5.66232677253651E-002
ITER=63	ERROR=+8.69765590127990E-002
ITER=64	ERROR=-1.57571994050783E-001
ITER=65	ERROR=+2.18273951114641E-001
ITER=66	ERROR=+4.61002517974950E-002
ITER=67	ERROR=-4.34095887431083E-002
ITER=68	ERROR=+4.07719354531788E-002
ITER=69	ERROR=+3.66710794604408E-002
ITER=70	ERROR=+3.58025320207473E-002
ITER=71	ERROR=+4.99229799444528E-002
ITER=72	ERROR=+4.29717328093476E-002
ITER=73	ERROR=+3.02638578035917E-002
ITER=74	ERROR=+2.14248542172881E-002
ITER=75	ERROR=+1.29470819620268E-002
ITER=76	ERROR=+1.01245372480577E-002
ITER=77	ERROR=+1.60491731739915E-002
ITER=78	ERROR=+1.41255173710620E-002

ITER=80 ERROR=+3.275765372006704E-002
 ITER=81 ERROR=+3.21263520751197E-002
 ITER=82 ERROR=+7.85060658660657E-002
 ITER=83 ERROR=+4.84016653152273E-002
 ITER=84 ERROR=+8.00292309830918E-002
 ITER=85 ERROR=+6.49071228082659E-002
 ITER=86 ERROR=+2.79351874097461E-001
 ITER=87 ERROR=+7.21765644381938E-001
 ITER=88 ERROR=+1.73025615699822E-001
 ITER=89 ERROR=+1.14763319543632E-001
 ITER=90 ERROR=+3.58919685444346E-002
 ITER=91 ERROR=+4.70702618209133E-002
 ITER=92 ERROR=+3.21496447501316E-002
 ITER=93 ERROR=+3.09370687939432E-002
 ITER=94 ERROR=+2.31559111334462E-002
 ITER=95 ERROR=+1.79544365212953E-002
 ITER=96 ERROR=+1.36371453823398E-002
 ITER=97 ERROR=+7.37833935380434E-003

SLUR CG EXITED

OPTIONS ACTIVE IN THIS SLURPROGRAM:

0. EXIT PROGRAM

3. DEVELOP COMPLEX-VALUED AMPLITUDES. CONDITIONED ON GIVEN
 INPUT, WHERE CONDITIONING INPUT IS LESS THAN N.
 (USES OUTPUT FROM STEP #2.)

9. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

DO YOU WANT TO SAVE THE OUTPUT FROM LAST OPTION
 STEP IN A SEPARATE USER SPECIFIED FILE ? Y OR N

PLEASE ENTER THE FILE NAME FOR STORAGE

010073.DAT **OUTPUT FILE**

Programmed STOP

E)

CONSOLE LIST FOR OPTION NO. 5 WITH OUT3.DAT AS INPUT

PROGRAM SIMULATES WAVE PROPERTIES BY FREQUENCY DOMAIN METHODS
FOR EITHER UNCONDITIONAL OR CONDITIONAL SIMULATIONS.
(WRITTEN BY LEON BORGMAN, LARAMIE, WYOMING)

PLEASE KEY RETURN TO CONTINUE

DO YOU WISH TO READ OUTPUT FROM PREVIOUS RUNS
OF OPTIONS #1. OR #2? (Y = YES, N = NO
Y

WHAT IS THE FILE NAME FOR PREVIOUS OUTPUT?

OUT3.DAT **INPUT**

OPTIONS ACTIVE IN THIS SUBPROGRAM:

0. EXIT PROGRAM
1. PRODUCE COMPLEX AMPLITUDES FOR UNCONDITIONAL SIMULATIONS
2. PRE-PROCESS DATA TO PRODUCE NECESSARY INPUT FOR A
CONDITIONAL SIMULATION
3. SIMULATE TIME SERIES FROM AMPLITUDES (USES OUTPUT FROM
STEP #1. #3. OR #4.)
4. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

5 **OPTION NO.**

ENTER NOISE TO SIGNAL RATIO, AS RATIO OF NOISE
STANDARD DEVIATION TO SIGNAL STANDARD DEVIATION

0.0

CHANNEL NUMBER: 1

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.2

CHANNEL NUMBER: 2

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.0

CHANNEL NUMBER: 3

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.0

ENTER TIME STEP FOR START OF LIST AND RETURN

1

ENTER TIME STEP AT TERMINATION OF LIST AND RETURN

200

ENTER 0 IF GRAPHICAL OUTPUT IS DESIRED

KEY 1 IF NUMERICAL LIST OF TIME SERIES IS WANTED

1

NUMBER OF DEGREES OF FREEDOM = 0

FOR A CONSTANT TIME OF OBSERVATION.

4. PRE-PROCESS DATA TO PRODUCE NECESSARY INPUT FOR A
CONDITIONAL SIMULATION
5. SIMULATE TIME SERIES FROM AMPLITUDES (USES OUTPUT FROM
STEP #1, #3, OR #4.)
6. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

3
DO YOU WANT TO SAVE THE OUTPUT FROM LAST OPTION
STEP ON A SEPARATE USER SPECIFIED FILE ? Y OR N

4
Programmed STOP

5)

LSIM4

CONSOLE LIST OPTION NO. 4

PROGRAM SIMULATES WAVE PROPERTIES BY FREQUENCY DOMAIN METHODS
FOR EITHER UNCONDITIONAL OR CONDITIONAL SIMULATIONS.
(WRITTEN BY LEON BORGMAN, LARAMIE, WYOMING)

PLEASE KEY RETURN TO CONTINUE

DO YOU WISH TO READ OUTPUT FROM PREVIOUS RUNS
OF OPTIONS #1 OR #2? (Y = YES, N = NO)

Y

WHAT IS THE FILE NAME FOR PREVIOUS OUTPUT?

J:OUT8.DAT ← INPUT

TITLE: 5/23/88

DOCUMENTATION: 6:20 PM

ISEED= 12345677 ICHU2= 2 N= 512 NTS= 1

OPTIONS ACTIVE IN THIS SUBPROGRAM:/' 2. EXIT PROGRAM

4. DEVELOP COMPLEX-VALUED AMPLITUDES. CONDITIONED ON GIVEN

INPUT. WHERE CONDITIONING INTERVAL EQUALS N.

(USES OUTPUT FROM STEP #2.)

8. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

4 ← OPTION NO.

THE GIVEN TIME SERIES IS TO BE READ FROM WHAT FILE?

J:GTS4.DAT

OPTION 4: JM=1
OPTION 4: JM=2
OPTION 4: JM=3
OPTION 4: JM=4
OPTION 4: JM=5
OPTION 4: JM=6
OPTION 4: JM=7
OPTION 4: JM=8
OPTION 4: JM=9
OPTION 4: JM=10
OPTION 4: JM=11
OPTION 4: JM=12
OPTION 4: JM=13
OPTION 4: JM=14
OPTION 4: JM=15
OPTION 4: JM=16
OPTION 4: JM=17
OPTION 4: JM=18
OPTION 4: JM=19
OPTION 4: JM=20

These can easily be removed from
FORTRAN code.

However, it is pleasant to see on
the console that the computer
is moving along in the calculations.

OPTION 4: JM=23
OPTION 4: JM=24
OPTION 4: JM=25
OPTION 4: JM=26
OPTION 4: JM=27
OPTION 4: JM=28
OPTION 4: JM=29
OPTION 4: JM=30
OPTION 4: JM=31
OPTION 4: JM=32
OPTION 4: JM=33
OPTION 4: JM=34
OPTION 4: JM=35
OPTION 4: JM=36
OPTION 4: JM=37
OPTION 4: JM=38
OPTION 4: JM=39
OPTION 4: JM=40
OPTION 4: JM=41
OPTION 4: JM=42
OPTION 4: JM=43
OPTION 4: JM=44
OPTION 4: JM=45
OPTION 4: JM=46
OPTION 4: JM=47
OPTION 4: JM=48
OPTION 4: JM=49
OPTION 4: JM=50
OPTION 4: JM=51
OPTION 4: JM=52
OPTION 4: JM=53
OPTION 4: JM=54
OPTION 4: JM=55
OPTION 4: JM=56
OPTION 4: JM=57
OPTION 4: JM=58
OPTION 4: JM=59
OPTION 4: JM=60
OPTION 4: JM=61
OPTION 4: JM=62
OPTION 4: JM=63
OPTION 4: JM=64
OPTION 4: JM=65
OPTION 4: JM=66
OPTION 4: JM=67
OPTION 4: JM=68
OPTION 4: JM=69
OPTION 4: JM=70
OPTION 4: JM=71
OPTION 4: JM=72
OPTION 4: JM=73
OPTION 4: JM=74
OPTION 4: JM=75
OPTION 4: JM=76
OPTION 4: JM=77
OPTION 4: JM=78
OPTION 4: JM=79
OPTION 4: JM=80
OPTION 4: JM=81
OPTION 4: JM=82
OPTION 4: JM=83
OPTION 4: JM=84
OPTION 4: JM=85
OPTION 4: JM=86

OPTION 4: JM=88
 OPTION 4: JM=89
 OPTION 4: JM=90
 OPTION 4: JM=91
 OPTION 4: JM=92
 OPTION 4: JM=93
 OPTION 4: JM=94
 OPTION 4: JM=95
 OPTION 4: JM=96
 OPTION 4: JM=97
 OPTION 4: JM=98
 OPTION 4: JM=99
 OPTION 4: JM=100
 OPTION 4: JM=101
 OPTION 4: JM=102
 OPTION 4: JM=103
 OPTION 4: JM=104
 OPTION 4: JM=105
 OPTION 4: JM=106
 OPTION 4: JM=107
 OPTION 4: JM=108
 OPTION 4: JM=109
 OPTION 4: JM=110
 OPTION 4: JM=111
 OPTION 4: JM=112
 OPTION 4: JM=113
 OPTION 4: JM=114
 OPTION 4: JM=115
 OPTION 4: JM=116
 OPTION 4: JM=117
 OPTION 4: JM=118
 OPTION 4: JM=119
 OPTION 4: JM=120
 OPTION 4: JM=121
 OPTION 4: JM=122
 OPTION 4: JM=123
 OPTION 4: JM=124
 OPTION 4: JM=125
 OPTION 4: JM=126
 OPTION 4: JM=127

OPTIONS ACTIVE IN THIS SUBPROGRAM:/' 0. EXIT PROGRAM
 4. DEVELOP COMPLEX-VALUED AMPLITUDES, CONDITIONED ON GIVEN
 INPUT, WHERE CONDITIONING INTERVAL EQUALS N.
 (USES OUTPUT FROM STEP #2.)

8. HELP

 (PLEASE ENTER YOUR CHOICE AND KEY RETURN)

0
 DO YOU WANT TO SAVE THE OUTPUT FROM LAST OPTION
 STEP ON A SEPARATE USER SPECIFIED FILE ? Y OR N

Y
 PLEASE ENTER THE FILE NAME FOR STORAGE
 J:OUT4.DAT **OUTPUT FILE**

Programmed STOP

F>

L:SIM125

**CONSOLE LIST FOR OPTION NO. 5
USING OUT4.DAT AS INPUT**

PROGRAM SIMULATES WAVE PROPERTIES BY FREQUENCY DOMAIN METHODS
FOR EITHER UNCONDITIONAL OR CONDITIONAL SIMULATIONS.
(WRITTEN BY LEON BORGMAN, LARAMIE, WYOMING)

PLEASE KEY RETURN TO CONTINUE

DO YOU WISH TO READ OUTPUT FROM PREVIOUS RUNS
OF OPTIONS #1 OR #2? (Y = YES, N = NO
Y

WHAT IS THE FILE NAME FOR PREVIOUS OUTPUT?

J:OUT4.DAT **INPUT**

OPTIONS ACTIVE IN THIS SUBPROGRAM:

- 0. EXIT PROGRAM
- 1. PRODUCE COMPLEX AMPLITUDES FOR UNCONDITIONAL SIMULATIONS
- 2. PRE-PROCESS DATA TO PRODUCE NECESSARY INPUT FOR A
CONDITIONAL SIMULATION
- 5. SIMULATE TIME SERIES FROM AMPLITUDES (USES OUTPUT FROM
STEP #1, #3, OR #4.)
- 8. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

5 . OPTION NO.

ENTER NOISE TO SIGNAL RATIO. AS RATIO OF NOISE
STANDARD DEVIATION TO SIGNAL STANDARD DEVIATION

0.0

CHANNEL NUMBER: 1

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.0

CHANNEL NUMBER: 2

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.0

CHANNEL NUMBER: 3

PLEASE ENTER MEAN VALUE DESIRED FOR THIS CHANNEL

0.0

ENTER TIME STEP FOR START OF LIST AND RETURN

1

ENTER TIME STEP AT TERMINATION OF LIST AND RETURN

200

ENTER 0 IF GRAPHICAL OUTPUT IS DESIRED

KEY 1 IF NUMERICAL LIST OF TIME SERIES IS WANTED

1

NUMBER OF DEGREES OF FREEDOM = 0

1. PRODUCE COMPLEX ANALY. USED FOR UNCONDITIONAL SIMULATIONS
2. PRE-PROCESS DATA TO PRODUCE NECESSARY INPUT FOR A
CONDITIONAL SIMULATION
5. SIMULATE TIME SERIES FROM AMPLITUDES (USES OUTPUT FROM
STEP #1, #3, OR #4.)
8. HELP

(PLEASE ENTER YOUR CHOICE AND KEY RETURN)

DO YOU WANT TO SAVE THE OUTPUT FROM LAST OPTION
STEP ON A SEPARATE USER SPECIFIED FILE ? Y OR N
N

Programmed STOP

F)

**Time series are stored in printer
listing LIST45.DAT**

-:SIM7

CONSOLE LIST OPTION NO. 7

PROGRAM SIMULATES WAVE PROPERTIES BY FREQUENCY DOMAIN METHODS
FOR EITHER UNCONDITIONAL OR CONDITIONAL SIMULATIONS.
(WRITTEN BY LEON BORGMAN, LARAMIE, WYOMING)

PLEASE KEY RETURN TO CONTINUE

DO YOU WISH TO READ OUTPUT FROM PREVIOUS RUNS
AS INPUT FOR THIS RUN? (Y = YES, N = NO)

Y

WHAT IS THE FILE NAME FOR THIS INPUT?

J:OUT4.DAT ← **INPUT**

OPTIONS ACTIVE IN THIS SUBPROGRAM:

0. EXIT PROGRAM

7. PRODUCE A REDUCED SET OF AMPLITUDES FOR A LOW RESOLUTION
REPRESENTATION THE SEA SURFACE AND KINEMATICS.
(USES OUTPUT FROM STEPS #1 OR STEP #3.)

8. HELP

(PLEASE KEY YOUR CHOICE AND RETURN)

7 ← **OPTION NO.**

PLEASE ENTER THE LOWEST AMPLITUDE OF INTEREST

0.1

QWKSRT

DO YOU WANT TO SEE A COMPARISON OF THE FULL
RESOLUTION AND THE LOW RESOLUTION WAVE TIME HISTORIES
AT X=0, Y=0 ? (Y OR N)

Y

ENTER TIME STEP FOR START OF LIST AND RETURN

1

ENTER TIME STEP AT TERMINATION OF LIST AND RETURN

200

ENTER 0 IF GRAPHICAL OUTPUT IS DESIRED

KEY 1 IF NUMERICAL LIST OF TIME SERIES IS WANTED

0

OPTIONS ACTIVE IN THIS SUBPROGRAM:

0. EXIT PROGRAM

7. PRODUCE A REDUCED SET OF AMPLITUDES FOR A LOW RESOLUTION
REPRESENTATION THE SEA SURFACE AND KINEMATICS.
(USES OUTPUT FROM STEPS #1 OR STEP #3.)

8. HELP

(PLEASE KEY YOUR CHOICE AND RETURN)

DO YOU WANT TO SEE THE OUTPUT FROM LAST OPTION?

Programmed STOP

F>

**List of low resolution amplitudes is
printed on line printer as shown in LIST7.DAT.**

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